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# **Energetics of Donor-Doping, Metal Vacancies,** and Oxygen-Loss in A-Site Rare-Earth-Doped BaTiO<sub>3</sub>

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The energetics of La-doping in BaTiO<sub>3</sub> are reported for both (electronic) donor-doping with the creation of Ti<sup>3+</sup> cations and ionic doping with the creation of Ti vacancies. The experiments (for samples prepared in air) and simulations demonstrate that ionic doping is the preferred mechanism for all concentrations of La-doping. The apparent disagreement with electrical conduction of these ionic doped samples is explained by subsequent oxygenloss, which leads to the creation of Ti3+ cations. Simulations show that oxygen-loss is much more favorable in the ionic-doped system than undoped BaTiO<sub>3</sub> due to the unique local structure created around the defect site. These findings resolve the so-called "donor-doping" anomaly in BaTiO<sub>3</sub> and explain the source of semiconductivity in positive temperature coefficient of resistance (PTCR) BaTiO<sub>3</sub> thermistors.

#### 1. Introduction

#### 1.1. Rare-Earth Doping in BaTiO<sub>3</sub>

Trivalent rare earth (RE) ions are commonly used to modify the electrical properties of ferroelectric perovskite BaTiO<sub>3</sub> (ABO<sub>3</sub>) ceramics in applications such as multi-layer ceramic capacitors (MLCCs)<sup>[1]</sup> and positive temperature coefficient of resistance (PTCR) thermistors.<sup>[2]</sup> Due to the intermediate size and charge of the RE<sup>3+</sup> ions compared to the Ba<sup>2+</sup>and Ti<sup>4+</sup> ions, several aliovalent doping mechanisms (ionic and electronic) are plausible. In general, based on ion size effects, small RE<sup>3+</sup> ions such as Yb3+ dope exclusively on the B-site with charge compensation by oxygen vacancies (Ba[Ti<sub>1-h</sub>RE<sub>h</sub>]O<sub>3-h/2</sub>), intermediate sized RE<sup>3+</sup> ions such as Gd<sup>3+</sup> can dope simultaneously onto the Aand B-sites (so-called self compensation, [Ba<sub>1-a</sub>RE<sub>a</sub>][Ti<sub>1-b</sub>RE<sub>b</sub>]O<sub>3</sub>)

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DOI: 10.1002/adfm.201203147



and large RE3+ ions such as La dope exclusively on the A-site.[3] In many cases, however, the doping mechanism(s) are also dependent on processing parameters such as the oxygen partial pressure  $(pO_2)$ , sintering temperature/time and the overall A/B ratio in the formulation of the device.[1] The situation is further complicated as commercial devices are heterogeneous and deliberately prepared under non equilibrium conditions to optimize/ control the desired electrical properties. For example, short sintering times are employed in MLCCs to ensure limited diffusion of dopants such as RE3+ ions into the grains to create so-called grain coreshell microstructures that are required

to modify the temperature dependence of the permittivity and therefore capacitance of the device.<sup>[1]</sup> In the case of semiconducting PTCR-BaTiO<sub>3</sub> thermistors, low levels (<<1 at%) of RE<sup>3+</sup> doping occurs on the A-site and devices are cooled in air from the sintering temperature to allow limited (but necessary) uptake of oxygen along the grain boundaries. This is required to develop and/or enhance the Schottky barriers between the semiconducting grain-insulating grain boundary junctions to create such a non-ohmic device.[2]

A-site doping of RE3+ ions has been a challenging topic for many years with the room temperature dc resistivity of ceramics being either semiconducting or insulating depending on the level of dopant and/or ceramic processing conditions.[4-10] A schematic diagram of the dc (total) resistivity of A-site doped RE<sup>3+</sup>-BaTiO<sub>2</sub> ceramics processed in air at ≈1400 °C is shown in Figure 1. The resistivity decreases by greater than 8 orders of magnitude with low levels of doping (<<1 at%) to yield semiconducting ceramics; however, the dc resistivity becomes insulating with higher doping levels (solid line, Figure 1). A popular interpretation of this result for RE = La, based on dc conductivity experiments of ceramics<sup>[4–6,11]</sup> and atomistic simulations of Lewis and Catlow,[12] is that there is a switch in the doping mechanism with increasing doping level. At low dopant levels an electronic (donor doping) mechanism occurs to induce the semiconductivity but there is a switch to an ionic compensation mechanism at higher doping levels to re-establish the insulating behavior. [4-6] The arrow in Figure 1 indicates A-site RE<sup>3+</sup> doping levels that are used on an industrial scale to produce PTCR thermistors (typically 0.2 to 0.5 at%). In recent years, we have questioned this interpretation of Figure 1 and in particular, the need for a magic switch in the doping mechanism.<sup>[13]</sup>

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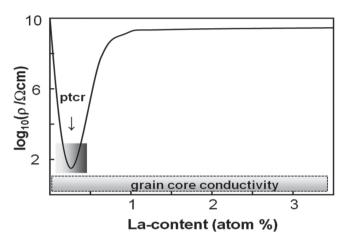


Figure 1. Schematic diagram showing the variation in dc resistivity of La-doped BaTiO<sub>3</sub> ceramics processed in air at 1400 °C followed by rapid cooling to room temperature (solid black line). Dashed and vertically shaded box indicates the range of the lowest grain core resistivity values obtained from impedance spectroscopy. The range of compositions suitable for PTCR thermistors is indicated by the horizontally shaded box.

### 1.2. La-Doping

Due to its large size, La is unique as a RE3+ dopant in BaTiO3 as it substitutes only on the A-site; [7-10,14,15] self-compensation and/or B-site doping do not occur. There are three plausible A-site doping mechanisms; 3 Ba<sup>2+</sup>  $\rightarrow$  2 La<sup>3+</sup> with the creation the creation of Ti-site vacancies (Ba<sub>1-v</sub>La<sub>v</sub>Ti<sub>1-v/4</sub>O<sub>3</sub>); and, socalled donor-doping via the electronic compensation mechanism  $Ba^{2+} \rightarrow La^{3+} + e^{-}$  ( $Ba_{1-z}La_{z}TiO_{3}$ ). Several experimental phase diagram studies for samples prepared in air according to the various A-site compensation mechanisms have all shown the favored mechanism to be the creation of Ti-site vacancies  $(V_{T_i})^{1/1/1}$  with an extensive solid solution limit of  $v \approx 0.20$ 0.25.[10,14,15] There is no experimental evidence for the existence of the Ba-vacancy or donor-doping mechanism(s), at least down to the detection limits of the techniques employed in the reported phase-diagram studies, i.e., X-ray diffraction and analytical electron microscopy. Samples prepared according to the donor-doping mechanism give phase mixtures of  $Ba_{1-\nu}La_{\nu}Ti_{1-\nu/4}O_3$  and other Ti-rich phase(s) such as Ba<sub>6</sub>Ti<sub>17</sub>O<sub>40</sub>.<sup>[8]</sup> Due to the immobility of metal vacancies at ambient conditions all  $Ba_{1-\nu}La_{\nu}Ti_{1-\nu/4}O_3$ prepared in air are expected to be room temperature electrical insulators.[16]

The problem, however, is that the electrical properties of Ladoped BaTiO $_3$  ceramics (and that of other A-site RE $^{3+}$  doped materials such as Gd, Ho, Dy) are very dependent on the processing conditions such as the oxygen partial pressure, the sintering temperature and the rate of cooling from the sintering temperature. For example, sintering (and subsequent cooling) all single-phase Ba $_{1-\gamma}$ La $_{\gamma}$ Ti $_{1-\gamma/4}$ O $_3$  compositions at 1400 °C in flowing oxygen results in electrically homogeneous ceramics. Impedance spectroscopy (IS) reveals the grain and grain boundary regions to be electrically insulating (>10 $^8$   $\Omega$  cm) at room temperature irrespective of y and there is no anomaly between the doping mechanism observed by the equilibrium

phase diagram studies and the measured electrical properties. [9] Sintering (and subsequent cooling) all single-phase Ba<sub>1-v</sub>La<sub>v</sub>Ti<sub>1-v/4</sub>O<sub>3</sub> samples at 1400 °C in air, however, results in electrically heterogeneous ceramics. [9,10,13] IS reveals two extreme types of electrical microstructures that are dependent on y and/or the ceramic microstructure of the ceramics.<sup>[9]</sup> In some cases, usually for small values of y (<<0.01), the grains are semiconducting and the grain boundaries are insulating and this can give rise to the very useful PTCR effect for thermistor applications (see arrow in Figure 1). In other cases, usually for larger values of y (>0.01), the outer regions (skin or surface layer) of the ceramic are electrically insulating at room temperature whereas the inner regions (core) of the ceramic remain semiconducting. In all cases, the samples remained single phase but IS reveals that the room temperature grain resistivity varies from  $\approx 10$  to  $>10^8$   $\Omega$  cm for the same value of y depending on the processing atmosphere (air or oxygen, respectively) or the region of the ceramic studied (inner or outer regions, respectively). It is clear, therefore, that thermodynamics and kinetics can both play an important role in shaping the electrical properties of these materials.

These results led us to conclude that (electronic) donor-doping of BaTiO<sub>3</sub> with La (or any other trivalent RE<sup>3+</sup> doped on the A-site) was not a feasible doping mechanism for samples prepared in air and was not the source of the semiconductivity. [13] Instead, we proposed the favored doping mechanism to be the creation of Ti vacancies, i.e., Ba<sub>1-y</sub>La<sub>y</sub>Ti<sub>1-y/4</sub>O<sub>3</sub> and the source of semiconductivity to be the loss of a small amount of oxygen that occurs when sintering such compositions in air at high temperatures, i.e.,

$$O^{2-} \rightarrow \frac{1}{2}O_2(g) + 2e^-$$
 (1)

with the electrons being transferred to partially reduce some of the Ti<sup>4+</sup> (d<sup>0</sup>) to Ti<sup>3+</sup> (d<sup>1</sup>) ions.<sup>[13]</sup> The general formula could therefore be written as  $Ba_{1-\gamma}La_{\gamma}Ti_{1-\gamma/4}O_{3-\delta}$  where  $\delta$  represents the oxygen loss. Based on the equation for conductivity,  $\sigma =$ ngμ, with the lowest room temperature grain core resistivity of  $\approx$ 10  $\Omega$  cm (see shaded box with dashed line in Figure 1) and a mobility ( $\mu$ ) value of  $\approx 0.1-1.0$  cm<sup>2</sup>/(Vs)<sup>2</sup> [5,17,18] for BaTiO<sub>3</sub>, the carrier concentration (n) can be estimated to be  $\approx 6 \times 10^{16}$  to  $6 \times 10^{17} \text{ cm}^{-3}$  independent of y. This puts an upper limit on  $\delta$  to be  $\approx 0.0002$ . The observed electrical properties obtained for single-phase La-doped ceramics therefore depend on the sintering atmosphere, the cooling rate and the ceramic microstructure as this dictates the level and distribution of oxygen up-take on cooling. It should be noted that oxygen-loss is well known to induce semiconductivity in un-doped BaTiO3 when processed in inert or reducing atmospheres at temperatures above ≈1200 °C.[5]

## 2. Results and Discussion

#### 2.1. Computational Model

Our model to explain Figure 1 was still perceived to be controversial, especially as existing classical simulations by Buscaglia et al.<sup>[19]</sup> using a potential developed by Lewis and Catlow<sup>[12]</sup>

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Table 1 a) Solution energies for electronic (e') and ionic (V<sub>Ti</sub>////) doping mechanisms in La-doped BaTiO<sub>3</sub> based on models by Lewis and Catlow<sup>[12]</sup> and Freeman et al. [21] b) Solution energies for the electronic (e') and ionic (V<sub>T</sub>////) doping mechanisms in La-doped BaTiO<sub>3</sub> with 0.00 (infinite dilution), 0.04, 0.08 and 0.12 mole fraction of La<sup>3+</sup> on the A-site. Also shown are the energies of oxygen-loss and the creation of 2 Ti<sup>3+</sup> from the freed e/ in the pure BaTiO<sub>3</sub> lattice and in the presence of the ionic defect cluster. The binding energy of the oxygen vacancy and the La defect cluster is listed where a negative value indicates a preferred binding in the lattice. The energies for the defects with y = 0.04, 0.08 and 0.12 are calculated for the whole cluster, i.e., for all 4, 8 or 12  $La^+$  ions. The energies for the infinitely dilute case at y = 0.00 are calculated per  $La^{3+}$  ion.

a) Solution Energies	$La_{Ba}^{\bullet} + e^{f}$ (electronic compensation)		4 $La_{Ba}^{\bullet} + V_{Ti}^{////}$ (ionic compensation)	
	Lewis and Catlow <sup>[12]</sup> [eV] 0.22 <sup>a)</sup>	Freeman et al. <sup>[21]</sup> [eV] 9.06	Lewis and Catlow <sup>[12]</sup> [eV] 2.90 <sup>a)</sup>	Freeman et al. <sup>[21]</sup> [eV]
0% <sup>b)</sup> (eV)	4% [eV]	8% [eV]	12% [eV]	
4 La <sub>Ba</sub> * + V <sub>Ti</sub> //// (ionic compensation)	1.01	4.44	9.15	13.0
2 Ti <sub>Ti</sub> ' + V <sub>O</sub> ** (oxygen loss)	6.63	8.61	8.61	8.61
Binding Energy (defect cluster)	-4.29	-3.37	-7.03	-7.00
4 La <sub>Ba</sub> + $V_{Ti}$ //// + 2 Ti <sub>Ti</sub> / + $V_O$ (defect cluster)	3.23	9.68	10.73	14.61
$La_{Ba}$ * + $e$ / (electronic compensation)	9.06	12.24	24.44	36.98

<sup>&</sup>lt;sup>a)</sup>Taken from ref. [19]; <sup>b)</sup>0% refers to isolated defect calculations so the defects are at an infinite dilution.

suggested donor doping of La to be the lowest energy doping mechanism, at least for low levels of doping. Also, why should La-doping on the A-site facilitate oxygen-loss for samples prepared in air at >1200 °C? Prediction of the exact doping mechanisms and defect structures in doped BaTiO<sub>3</sub> is desirable and although a recent density functional theory (DFT) study<sup>[20]</sup> was in agreement with our experimental phase diagram for samples prepared in air and/or flowing O2 gas the cost of DFT simulations to study possible defect clusters and their segregation is prohibitively expensive.

The Lewis and Catlow model<sup>[12]</sup> was developed in the mid 1980s and was a completely ionic model. The origin of ferroelectricity in BaTiO<sub>3</sub> depends on the occurrence of covalency in the bonding between the Ti and O atoms. We have recently developed a new potential model for BaTiO<sub>3</sub><sup>[21]</sup> to account for this covalency by introduction of a lennard-jones potential and three-body terms to describe the interactions between the Ti and O. This new potential has produced much better agreement between experimental and calculated values for the lattice parameters and the cohesive energy of BaTiO<sub>3</sub> (a difference of <1%) as detailed in our previous publication.<sup>[21]</sup> Within this work we also presented a general discussion of the results for RE-doping in BaTiO<sub>3</sub>. A key result from this new model is the prohibitively large solution energy of all RE donor-doping compared to that reported by the Lewis and Catlow model. [12] For La-doping, our model predicts 9.06 eV compared to 0.22 eV based on the Lewis and Catlow model, see Table 1a. The solution energy of 1.01 eV for the Ti-vacancy (ionic) compensation mechanism for La at infinite dilution is much more favorable compared with 9.06 eV for donor-doping (electronic) compensation in this new model, Table 1a. Calculations have also been performed for y (ionic compensation) and z (electronic compensation) = 0.04, 0.08 and 0.12 (rows 3 and 7 in Table 1b, respectively) and in every case the solution energy is always

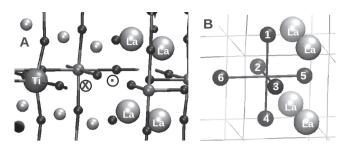
considerably lower for the Ti-vacancy mechanism. This result is in excellent agreement with the equilibrium phase diagram of La2O3-BaO-TiO2 for samples prepared in air and/or flowing oxygen and with a DFT study. [20] It is also in agreement with the insulating electrical properties of Ba<sub>1-v</sub>La<sub>v</sub>Ti<sub>1-v/4</sub>O<sub>3</sub> ceramics processed in flowing oxygen.<sup>[9,10]</sup> We now consider the energetics associated with oxygen-loss in doped BaTiO3 (Equation 1) to explain the source of semiconductivity in air sintered ceramics given the unfavorable solution energy associated with direct donor (electronic) doping.

## 2.2. Oxygen-Loss in Doped BaTiO<sub>3</sub>

The calculations show ≈6.63-8.61 eV is required to release oxygen from the undoped BaTiO<sub>3</sub> lattice to form V<sub>O</sub>" + 2 Ti<sub>Ti</sub>/ (oxygen loss, row 4, Table 1b). This energy is significantly reduced when oxygen loss is considered in the presence of the RE3+ defect cluster with binding energies of the oxygen vacancy cluster and RE<sup>3+</sup> cluster of ≈-4.29 to -7.00 eV (row 6, Table 1b). This clearly shows the overall energy associated with the oxygen-loss model for ionic compensation (defect cluster, row 5, Table 1b) is substantially lower when compared to direct donor doping of La (electronic compensation, row 7, Table 1b) and confirms this model as the source of the n-type semiconductivity in Ba<sub>1-v</sub>La<sub>v</sub>Ti<sub>1-v/4</sub>O<sub>3</sub> ceramics prepared in air at high temperatures.

Oxygen loss is energetically favored at the La-defect cluster due to the particular local structure for Ba<sub>0.96</sub>La<sub>0.04</sub>Ti<sub>0.99</sub>O<sub>3-δ</sub> (y = 0.04) that is shown in **Figure 2**. The lowest energy arrangement of the defects is with the Vo" occurring adjacent to the V<sub>Ti</sub>//// and surrounded by Ba<sup>2+</sup> A-site cations only, Figure 2a. The loss of the Ti reduces the local Madelung potential in the surrounding oxygen anions. Although the presence of the

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**Figure 2.** a) The relaxed structure of the defect sites in 4% La-doped BaTiO $_3$  by ionic compensation with 4 La $_{Ba}$  and Ti vacancies coupled with O loss to create Ti $^{3+}$  ions. Key: oxygen (dark grey); titanium (grey); barium (silver); lanthanum (labelled large silver); Ti $^{3+}$  (labelled large grey); V<sub>O</sub> (circle with cross); V<sub>Ti</sub> (circle with dot). b) Schematic diagram to show the removal of O(6) from Ba $_{1-\nu}$ La $_{\nu}$ Ti $_{1-\nu}$ Y $_{14}$ O $_3$ .

La<sub>Ba</sub> with a 3+ charge on each La will increase this potential for the oxygen anions that are nearest neighbor to these cations (labelled 1 to 5 in Figure 2b), for the single oxygen anion further away (labelled 6 in Figure 2b) the potential will be significantly diminished. Therefore there is a smaller energy penalty for this oxygen to exit the lattice compared to other oxygen anions. The electron compensation this causes within the lattice generates two  ${\rm Ti}^{3+}$  ions  $({\rm Ti}_{{\rm Ti}})$ . The first  ${\rm Ti}_{{\rm Ti}}$  is naturally preferred next to the  ${\rm V_O}$  due to the Coulomb attraction of the charged defect sites. The most favorable position of the second  ${\rm Ti}_{{\rm Ti}}$  is adjacent to the four La<sub>Ba</sub> as the reduction of the Ti here from 4+ to 3+ reduces the Coulombic repulsion between the cations.

#### 3. Conclusions

Millions of PTCR BaTiO<sub>3</sub> thermistors are produced annually for a wide variety of applications. Since the late 1960s, it has been widely accepted that the A-site RE<sup>3+</sup> doping required to produce semiconducting grains originates from direct donor-doping. The calculations presented here and in combination with previous experimental results<sup>[7–10,13]</sup> show this to be incorrect. Instead, the formation of titanium vacancies and the arrangement of the RE<sup>3+</sup> ions on the A-sites facilitate a mechanism for removal of oxygen anions from the lattice and this is the source of the semiconductivity for samples processed under the conditions commonly employed to manufacture PTCR BaTiO<sub>3</sub> thermistors.

#### 4. Methods

To explain the electrical properties of  $Ba_{1-y}La_yTi_{1-y/4}O_3$  ceramics prepared in air, calculations were performed that considered the solution energy for the creation of oxygen vacancies associated with oxygen loss from both pure  $BaTiO_3$  and doped  $Ba_1$ .  $_yLa_yTi_{1-y/4}O_3$  to form semiconducting  $Ba_{1-y}La_yTi_{1-y/4}O_{3-\delta}$  in the latter case. Static lattice minimization calculations were all performed with the GULP 3.1 code. [22] The defect energies were calculated using the Mott-Littleton two region approach. [23] Several potential defect clusters were considered and the lowest energy arrangement is reported. For the calculation of defect effects in y = 0.04, 0.08 and 0.12 a 100-formula unit cell was used (a  $5 \times 5 \times 4$  cell). The range of potential defect clusters was sampled using

four separate genetic algorithm (GA) runs on a group of twenty random starting populations of defect sites. The selectivity of breeding between successful populations was set at 50% and forty breeding rounds were attempted. The mutation rate was set at 10%. To reduce computational expense initial runs calculated only the single point energy of the cell. From these results twenty new populations were selected from the lowest energy configurations for four further GA runs using the same conditions, but now allowing for full optimization of the cell. The final optimized configuration was then identified from these four runs.

## Acknowledgements

The authors thank the EPSRC (EP/G005001/1) for funding. C.L.F. would like to thank EPSRC, grants (EP/I016589/1) and (EP/I001514/1) for additional funding.

Received: October 26, 2012 Revised: January 15, 2013 Published online: March 6, 2013

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